

# A 1D numerical model for incompressible fluids in pipes with variable section

Elena Travaglia

Ph.D. Modeling and Data Science  
Università degli studi di Torino

In collaboration with Ferrero s.p.a of Alba

Tutor: Matteo Semplice  
Università degli studi dell'Insubria

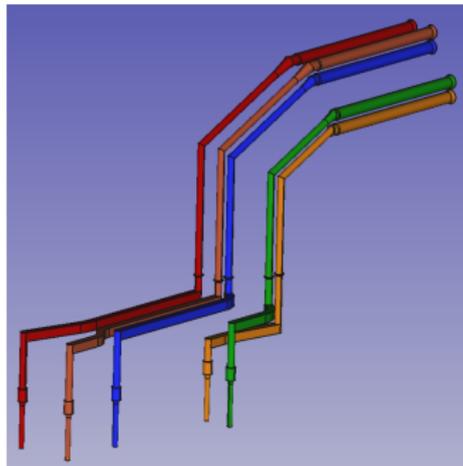
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# The industrial setting

We have an incompressible fluid and we want to compute the pressure drops in channels in a very efficient way.

Our task is to find a model

- with a very low computational cost.
- that represents all the fluid and the geometry characteristics.
- at least of third order of accuracy.



# Mathematical model

The mass and the momentum conservation equations are

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \bar{u}) = 0 \quad (1)$$

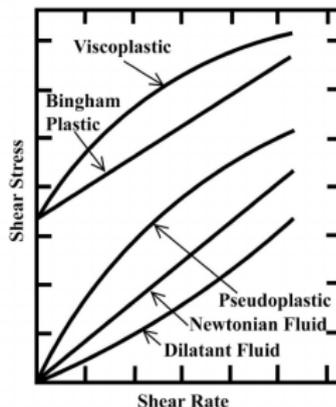
$$\rho \left( \frac{\partial \bar{u}}{\partial t} + (\bar{u} \cdot \nabla) \bar{u} \right) - \rho \mathbf{g} = -\nabla p + \nabla \cdot \sigma \quad (2)$$

Assumptions:

- incompressible fluid  $\rho = \text{const}$  so (1) becomes  $\nabla \cdot \bar{u} = 0$
- "no-slip" condition so  $\bar{u} = 0$  on solid boundary
- inlet : Dirichlet condition for  $\bar{u}$   
outlet: Neumann condition for  $p$ .

A fluid can be

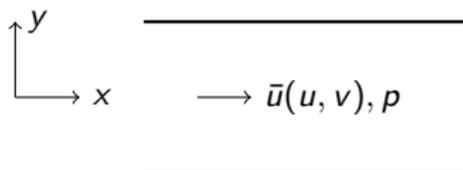
- Newtonian  $\sigma = \mu \bar{\gamma}$
- Non-Newtonian  $\sigma = \mu(\bar{\gamma}) \bar{\gamma}$   
where  $\bar{\gamma}$  is the tensor strain and it is defined as  $\bar{\gamma} = \nabla \bar{u} + (\nabla \bar{u})^T$



# NS analytic solution, Poiseuille

The incompressible Navier-Stokes equations:

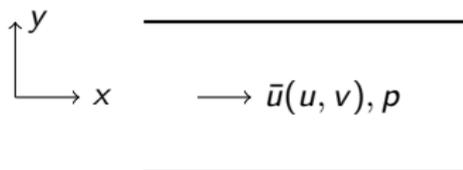
$$\begin{cases} \rho \left( \frac{\partial \bar{\mathbf{u}}}{\partial t} + (\bar{\mathbf{u}} \cdot \nabla) \bar{\mathbf{u}} \right) = -\nabla p + \nabla \cdot \sigma \\ \nabla \cdot \bar{\mathbf{u}} = 0 \end{cases}$$



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Hypothesis:

- the radius  $R$  is constant
- stationary solution
- fully developed flow

$\implies$

- $v = 0$
- $u(x) = \text{const}$

$$\implies \partial_y (\mu \partial_y u) = \partial_x p$$

elliptic eq. on the transverse direction

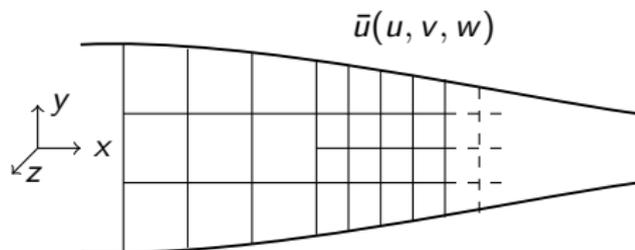


we obtain a velocity profile, that it is parabolic for a newtonian fluid

$$u(y) = \frac{\partial_x p}{4\mu} (R^2 - y^2)$$

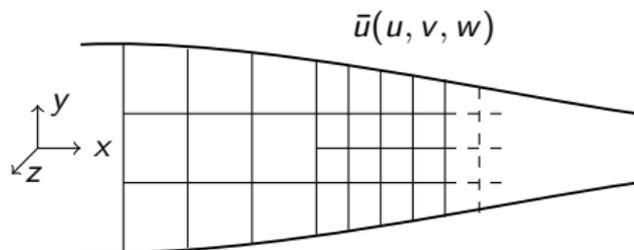
## If $R$ is non constant

- $v, w \neq 0$   
 $\Rightarrow \partial_y p \neq \partial_z p \neq 0$
- $u(x) \neq \text{constant}$
- $u(y) \neq \text{parabolic}$
- the pressure drop isn't constant  
 $\Rightarrow \partial_x p \neq \text{constant}$



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- the pressure drop isn't constant  
 $\Rightarrow \partial_x p \neq \text{constant}$



We could :

- use a 3D solver
- discretize in  $x$  and in the transversal directions
- approximate the solution with  $\mathbb{P}_g$  in each cell

**Problem:** it requires a high computational cost.

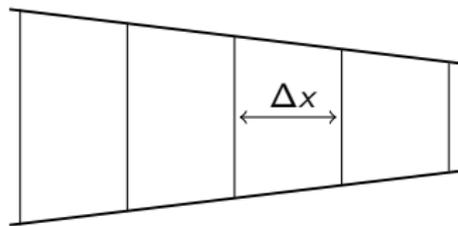
# Almost 1D approximation

**Idea:** we want to solve a 1D equation in the  $x$  direction, but we don't know how to analytically calculate the velocity profile, so we decide to compute it numerically.

We assume:

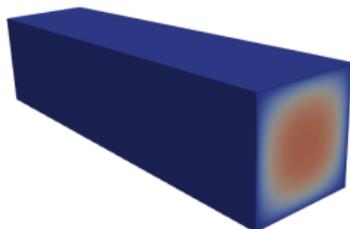
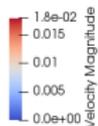
- slowly varying diameter of pipe
- $v, w = 0 \implies \frac{\partial p}{\partial y} = \frac{\partial p}{\partial z} = 0$
- $u = u(x, y, z)$  and  $u = 0$  on the boundary (no-slip)
- velocity: Dirichlet condition in inflow  
pressure:  $p - \sigma = p_{out}$  in outflow

**Main point:** we discretize only in  $x$  direction and we use a high polynomial degree in  $y$  and  $z$  directions to determine the profile (it is no longer parabolic)



# Pipe with rectangular section, for a non newtonian fluid

## OpenFoam comparison

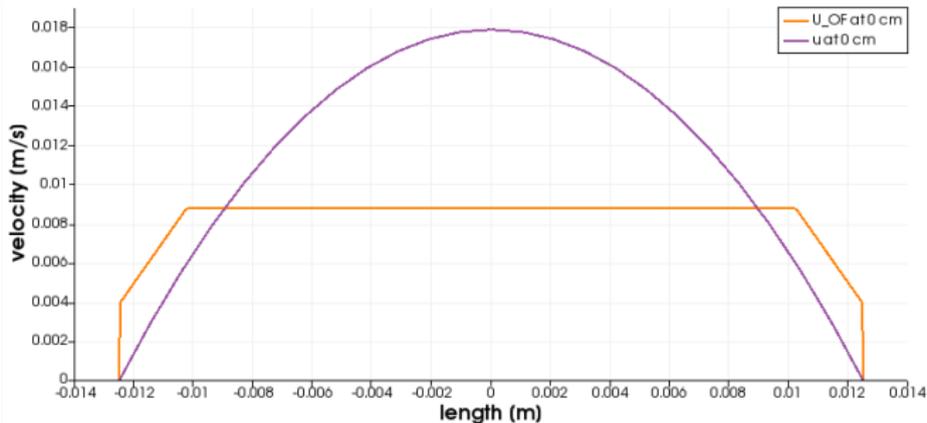


Geometry:

$$H_{in} = 2.5 \text{ cm} \quad L = 10 \text{ cm}$$

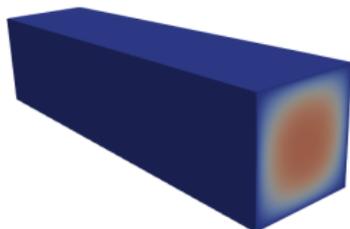
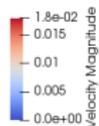
BC inlet:

- our program  
 $u = \text{parabolic}$
- Open Foam  
 $u = 0.0088 \text{ m s}^{-1}$



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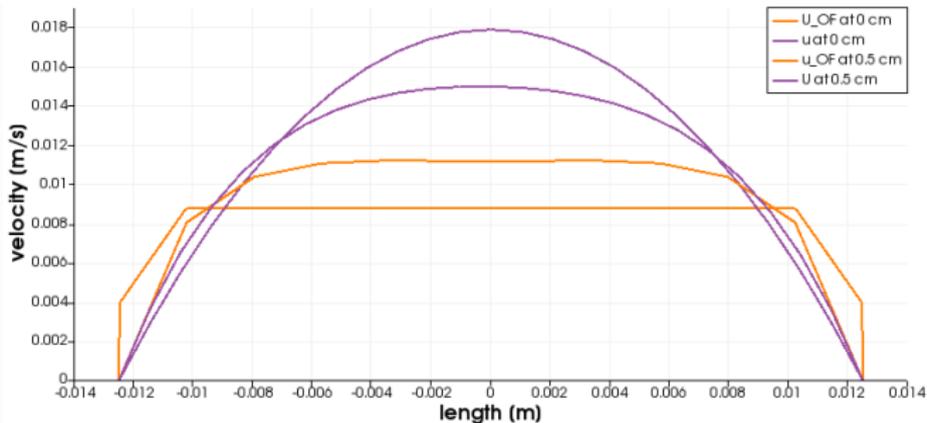


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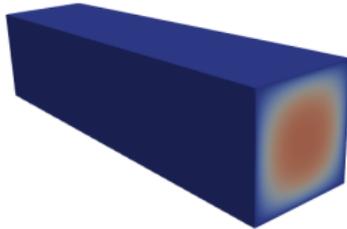
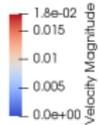
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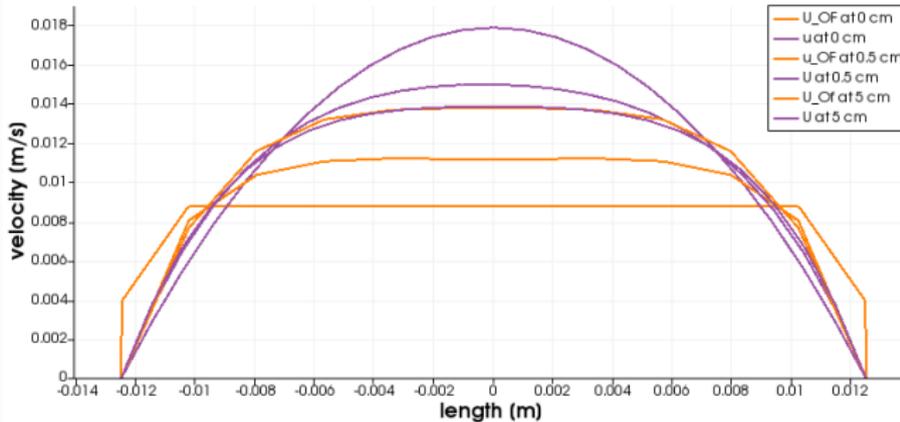


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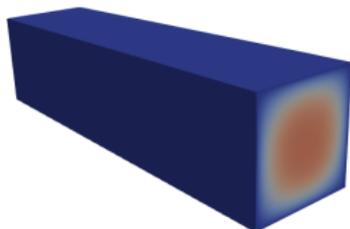
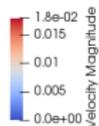
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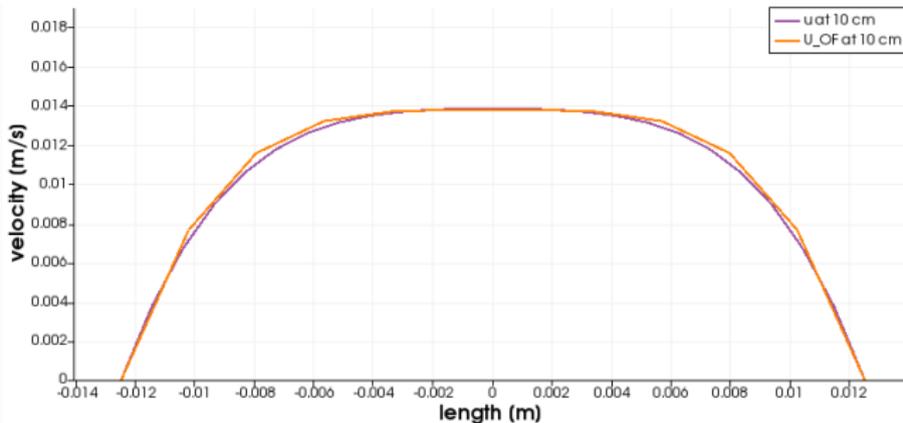


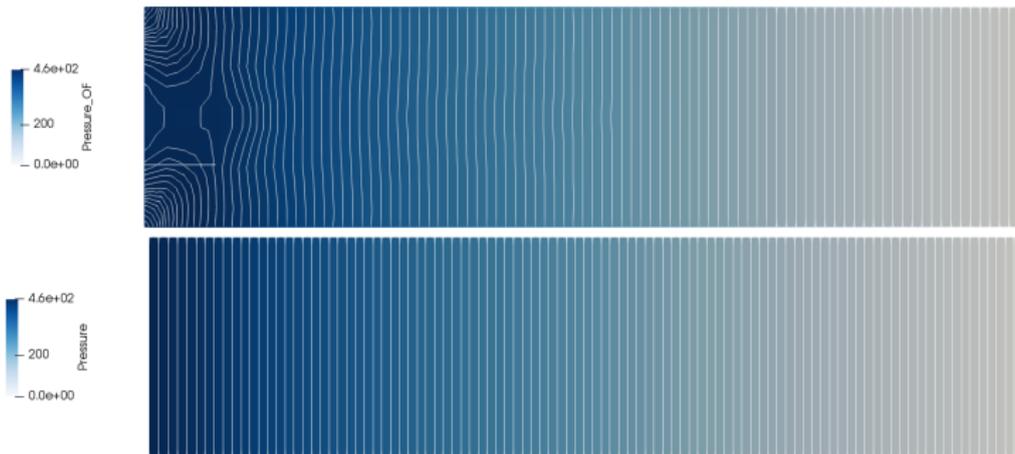
Geometry:

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BC inlet:

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 $u = \text{parabolic}$
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 $u = 0.0088 \text{ m s}^{-1}$





Comparing the average piston pressure, obtained with OpenFoam, there is a value 3% higher than that obtained with our model.

In a simulation with 80 cells, the CPU time for

- OpenFoam is 59 s
  - our program is 29 s
- with a reduction of 50%.

# Curved pipe with variable radius, for a non newtonian fluid

## OpenFoam comparison

Geometry:  $H_{in} = 2.5$  cm,  $H_{out} = 1.25$  cm,  $L = 10$  cm,  $\theta = \pi/3$

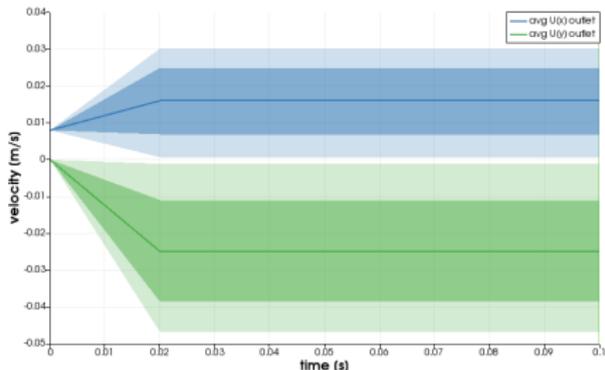
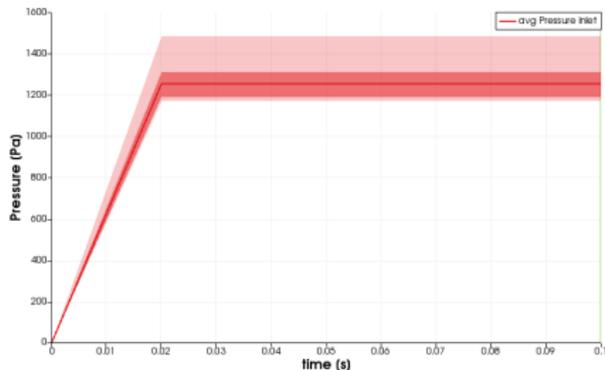


The average pressure, estimated by our program, is 7% lower than the average value on the inlet face for OpenFoam. Instead the axial velocity is 4% higher.

With 160 cells, the CPU time for

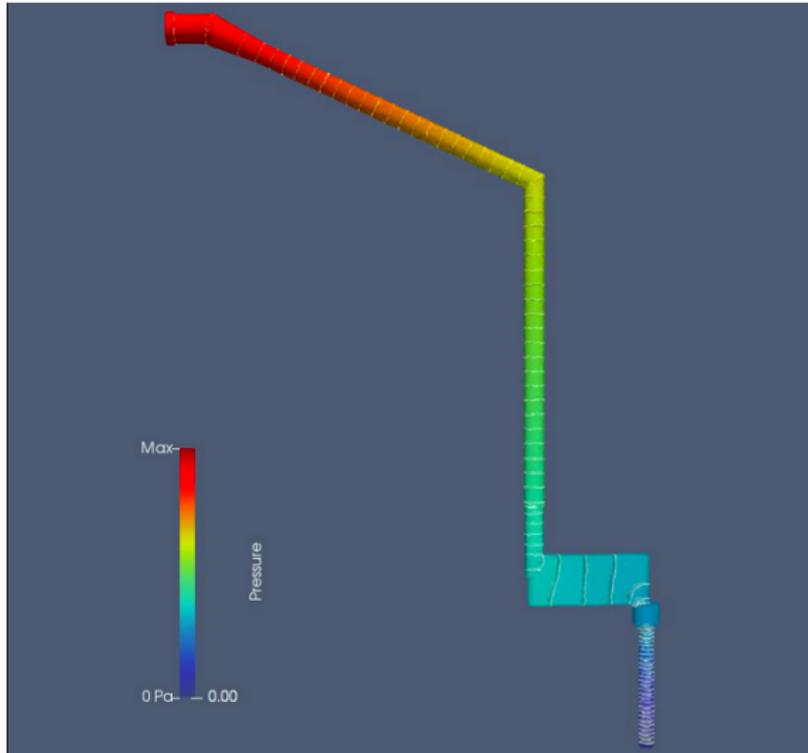
- OpenFoam is 8.35 min
- our program is 1.49 min

with a reduction of about 82%.



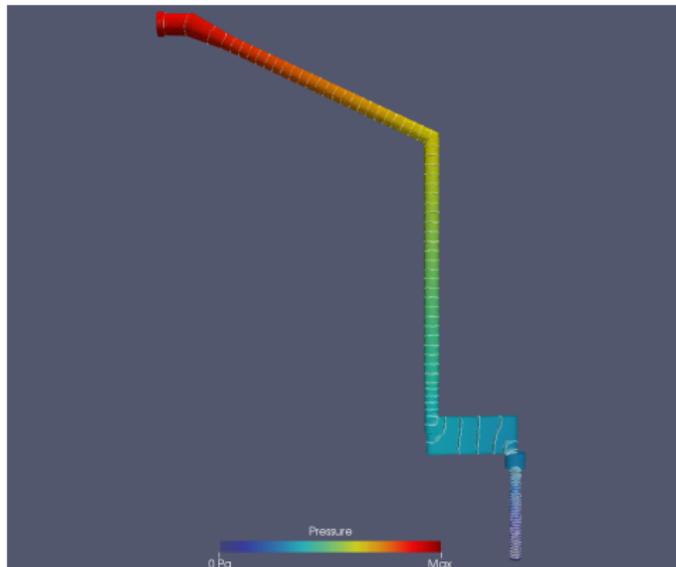
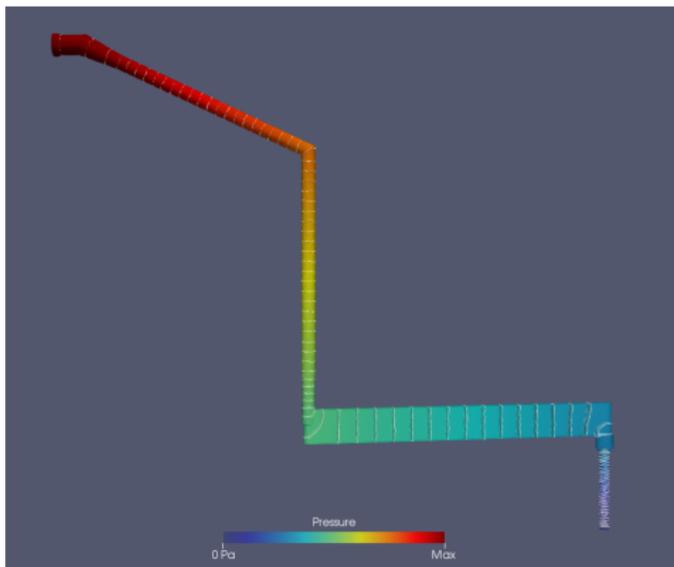
## Example

We simulate the behavior of a fluid being pushed into a channel by a moving wall. In the first 0.05 seconds the velocity is increased and then it is kept constant.



## Pipes comparison

Comparison between the pressure drops in two channels which differ only in the horizontal part.



The a priori simulation of the behavior of fluids is particularly useful in the design phase because it allows to create components that respect particular physical constraints.